

$$\textcircled{1} h = A_0 \frac{G}{c^2} \frac{I_0}{r} + A_1 \frac{G}{c^3} \frac{\dot{I}_1}{r} + A_2 \frac{G}{c^4} \frac{I_2}{r} + \dots +$$

$$+ B_1 \frac{G}{c^4} \frac{\dot{J}_1}{r} + B_2 \frac{G}{c^5} \frac{\ddot{J}_2}{r} \dots =$$

$$= \frac{G}{c^2 r} \sum_{l=0}^{\infty} \frac{A_l}{c^l} \frac{d^l I_l}{dt^l} + \frac{G}{c^4 r} \sum_{l=1}^{\infty} \frac{B_l}{c^{l-1}} \frac{d^l J_l}{dt^l} \quad (\#\#)$$

where A_l, B_l are real numbers.

$$\left[\frac{G}{c^2 r} \right] = \frac{M \cancel{L^2}}{\cancel{L^2} M^2} \left(\frac{L}{L} \right)^{-2} \frac{1}{\cancel{L}} = \frac{1}{M}$$

$$\left[\frac{G}{c^4 r} \right] = [c^{-2}] \left[\frac{G}{c^2 r} \right] = \frac{T^2}{L^2 M}$$

$$[I_l] \sim \left[\int x^l \rho d^3x \right] = ML^l$$

$$[J_l] \sim \left[\int x^l v \rho d^3x \right] = ML^l \frac{L}{T}$$

$$[h] = \left[\frac{G}{r c^2} \right] \sum_{l=0}^{\infty} \left[\frac{A_l}{c^l} \frac{d^l I_l}{dt^l} \right] + \left[\frac{G}{r c^4} \right] \sum_{l=1}^{\infty} \left[\frac{B_l}{c^{l-1}} \frac{d^l J_l}{dt^l} \right] =$$

$$= \frac{1}{M} \sum_{l=0}^{\infty} \frac{1}{L^l} \frac{1}{L^l} ML^l + \frac{T^2}{L^2 M} \sum_{l=1}^{\infty} \frac{1}{L^{l-1}} \frac{1}{T^l} ML^l \frac{L}{T}$$

dimensionless = $\frac{T^2}{L^2} \sum_{l=1}^{\infty} \frac{L^2}{T^l} \rightarrow$ dimensionless

$$\Rightarrow [h] = 1 \text{ dimensionless}$$

Consider the l -th term in the expansion; call it h_l , so that $h = \sum_l h_l$. Let's assume a generic term only depends on:

$$\left[\frac{G}{r} \right] = \frac{L^2}{MT^2}$$

$$\left[\frac{d^q}{dt^q} \right] = \frac{1}{T^q}$$

$$[I_l] = ML^l \quad \text{or} \quad [J_l] = \frac{ML^l}{T}$$

$$[c^\beta] = \frac{L^\beta}{T^\beta}, \text{ where } \alpha \geq 0, \gamma \geq 0.$$

So the dimensionality of the term is:

$$1) \left[\frac{G}{r} \right] \left[\frac{d^\alpha}{dt^\alpha} \right] [I_\gamma] [c^\beta] = \frac{L^2}{MT^2} \frac{1}{T^\alpha} ML^\gamma \frac{L^\beta}{T^\beta} = L^{\beta+\gamma+2} T^{-(\beta+\alpha+2)}$$

$$2) \left[\frac{G}{r} \right] \left[\frac{d^\alpha}{dt^\alpha} \right] [J_\gamma] [c^\beta] = \frac{L^2}{MT^2} \frac{1}{T^\alpha} ML^\gamma \frac{L}{T} \frac{L^\beta}{T^\beta} = L^{\beta+\gamma+3} T^{-(\beta+\alpha+3)}$$

Since h is adimensional, each term must be adimensional as well, which implies:

$$1) \begin{cases} \beta + \gamma + 2 = 0 \\ \beta + \alpha + 2 = 0 \end{cases}$$

$$\frac{\gamma - \alpha = 0}{\Rightarrow \begin{cases} \alpha = \gamma \\ \beta = -\gamma - 2 \end{cases}}$$

So the term is: $\frac{G}{r} \frac{d^\alpha}{dt^\alpha} I_\alpha \frac{1}{c^{\alpha+2}}$ with $\alpha \geq 0$

$$2) \begin{cases} \beta + \gamma + 3 = 0 \\ \beta + \alpha + 3 = 0 \end{cases}$$

$$\alpha = \gamma \text{ and } \beta = -\gamma - 3$$

so the term is: $\frac{G}{r} \frac{d^\alpha}{dt^\alpha} J_\alpha \frac{1}{c^{\alpha+3}}$ with $\alpha \geq 0$

$$\text{Replace now } \alpha \leftrightarrow l, \text{ then: } h = \sum_{l=0}^{\infty} \left[\frac{A_l}{c^2} \frac{G}{r} \frac{d^l I_l}{dt^l} \frac{1}{c^l} + \frac{B_l}{c^3} \frac{G}{r} \frac{d^l J_l}{dt^l} \frac{1}{c^l} \right]$$

with A_l, B_l dimensionless.

This is exactly (##); so we showed that dimensional analysis requires unambiguously form (##) for h .

$$\textcircled{2} \quad h \sim \frac{G}{c^4} \frac{\ddot{I}_2}{r} \sim \frac{G}{c^2} \frac{E_{\text{kin}}/c^2}{r}$$

• Meteorite

$$R = 10^3 \text{ m} \quad v = 25 \text{ km/s} = 25 \times 10^3 \text{ m/s}$$

$$\rho \sim 4000 \text{ kg/m}^3 \text{ (typical density from meteorites, wustl.edu)}$$

$$\Rightarrow M = \frac{4}{3} \pi R^3 \rho \cong 1.7 \times 10^{13} \text{ kg}$$

$$\begin{aligned} \ddot{I}_2 &\sim \int \rho(\vec{x}) x^2 d^3x \sim \int M \delta(x-vt) \delta(y) \delta(z) x^2 d^3x \\ &= M v^2 t^2 \quad \text{for a trajectory } \vec{x}_0(t) = vt \hat{x} \end{aligned}$$

$$\ddot{I}_2 \sim 2 M v^2 \sim E_{\text{kin}}$$

$$\boxed{r \sim \lambda} = \frac{c}{2\pi f} = \frac{cT}{2\pi} \quad \text{we must be at least } \lambda \text{ away from the source to be in the wave-zone}$$

$$T \sim \frac{R}{v} = 0.04 \text{ s} \Rightarrow \lambda \sim 2 \times 10^6 \text{ m}$$

$$\begin{aligned} h &\sim \frac{G}{c^2} \frac{E_{\text{kin}}/c^2}{\lambda} = \frac{6.67 \times 10^{-11}}{9 \times 10^{16}} \frac{1}{2 \times 10^6} \times \frac{2 \times 1.7 \times 10^{13} \times (25 \times 10^3)^2}{9 \times 10^{16}} \\ &= 8.7 \times 10^{-29} \sim 10^{-30} \quad \checkmark \end{aligned}$$

• Piezoelectric

$$f = 10^8 \text{ Hz}$$

$$\vec{x}_0(t) = A \cos(2\pi f t) \hat{x}, \quad \dot{\vec{x}}_0(t) = -2\pi f A \sin(2\pi f t) \hat{x}$$

$$\ddot{I}_2 \sim E_{\text{kin}} \cong \frac{1}{2} M |\dot{\vec{x}}_0(t)|^2 \sim \frac{1}{2} M (2\pi f A)^2$$

A large piezoelectric crystal I found advertised online was

$$M \sim 10 \text{ kg} \quad (\text{www.virtualaquariumshow.com/document/1193/brochure})$$

$$\text{with motions of the order of a few mm} \Rightarrow A \sim 1 \text{ mm} = 10^{-3} \text{ m}$$

$$\Rightarrow \frac{E_{\text{kin}}}{c^2} \sim \frac{1}{2} \times 10 \times 4\pi^2 \times 10^{16} \times 10^{-6} \frac{1}{9 \times 10^{16}} \text{ kg} = 2 \times 10^{-5} \text{ kg}$$

$$\lambda = \frac{c}{2\pi f}$$

$$\ddot{I}_2 = \frac{d^2}{dt^2} (M A^2 \cos^2(2\pi f t)) = -8 A^2 f^2 \pi^2 M \cos(4\pi f t)$$

$$T_{\text{GW}} = \frac{2\pi}{4\pi f} \Rightarrow \lambda = \frac{c}{2\pi} \frac{2\pi}{4\pi f} \cong 0.2 \text{ m}$$

$\frac{2\pi}{T_{\text{GW}}} \Rightarrow$

$$\frac{h}{c^2} \sim \frac{G}{c^2}$$

$$\frac{E_{\text{min}}/c^2}{t} = \frac{6.67 \times 10^{-11}}{9 \times 10^{18}}$$

$$\frac{2 \times 10^{-29}}{2 \times 10^{-11}} = 7 \times 10^{-22}$$



③ a) From Maggiore (4.224) and previous formulae, we have test for an ellipsoid which is rigidly rotating about its axis of symmetry with freq. ω_{rot} :

$$h_+ = \frac{4G\omega_{rot}^2}{c^4 r} (I_1 - I_2) \frac{1 + \cos^2 i}{2} \cos(2\omega_{rot} t) \quad (\#1)$$

$$h_x = \frac{4G\omega_{rot}^2}{c^4 r} (I_1 - I_2) \cos i \sin(2\omega_{rot} t)$$

where i is the angle b/w the line of sight and the rotation axis, I_1 and I_2 are the principal moments of inertia in the plane \perp rotation axis.

The deviation from ellipticity is defined as: $\epsilon \equiv \frac{I_1 - I_2}{I_3}$.

Note that $\omega_{GW} = 2\omega_{rot}$. Then

$$h_+ = h_0 \frac{1 + \cos^2 i}{2} \cos(\omega_{GW} t)$$

$$h_x = h_0 \cos i \sin(\omega_{GW} t)$$

$$\text{where } h_0 = \frac{4G\omega_{rot}^2}{c^4 r} \epsilon I_3 \stackrel{\omega_{rot} = \pi f_{GW}}{=} \frac{4G\pi^2 f_{GW}^2}{c^4 r} \epsilon I_3 \quad (\#2)$$

$$\text{So } h_{+x} \sim h_0 \propto f_{GW}^2 \quad \omega_{rot} = \pi f_{GW}$$

Let $\epsilon = 10^{-4}$, $I_3 \sim 10^{45} \text{ g cm}^2 = 10^{38} \text{ kg m}^2$.

$$1) f_{GW} = 10^2 \text{ Hz}$$

$$h_0 \approx \frac{33 \times 10^{-6} \text{ m}}{r}$$

$$\Rightarrow r \sim \frac{33 \times 10^{-6} \text{ m}}{10^{-21}} = 3.3 \times 10^{15} \text{ m} \approx 1 \text{ parsec} \quad \checkmark$$

$$2) f_{GW} = 10^3 \text{ Hz}$$

r is 100 larger than for $f_{GW} = 10^2 \text{ Hz}$, since $h_0 \propto f_{GW}^2$ then $r \sim 100 \text{ parsecs} \quad \checkmark$

For a more qualitative derivation of (#1) or (#2) see the following. For an ellipsoid with principal axes R , R and $R(1-\epsilon)$ the moment of inertia in the frame where the body is at rest and aligned with its principal axes is:

$$\mathbf{I}_{ij} = \begin{pmatrix} \frac{M}{5} [R^2 + R^2(1-\epsilon)] & 0 & 0 \\ 0 & \frac{M}{5} [R^2 + R^2(1-\epsilon)] & 0 \\ 0 & 0 & \frac{2}{5} MR^2 \end{pmatrix}$$

where $I_{ij} \equiv \int \rho(\vec{x}) (x^2 \delta_{ij} - x_i x_j) d^3x$.

In the quadrupole formula we have to take this to an inertial frame and do d^2/dt^2 . The trace part ($\sim x^2 \delta_{ij}$) is constant in time so we should look at the trace-free part only

$$I_{ij} - \frac{1}{3} \delta_{ij} \text{Tr}(I_{ab}) = \begin{pmatrix} -\frac{\epsilon MR^2}{15} & 0 & 0 \\ 0 & -\frac{\epsilon MR^2}{15} & 0 \\ 0 & 0 & \frac{2}{15} \epsilon MR^2 \end{pmatrix}$$

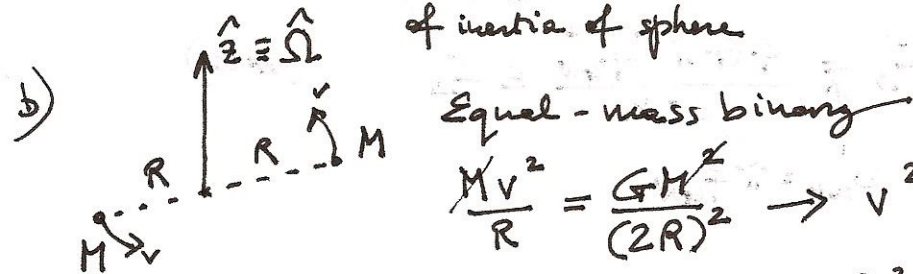
where we used $\text{Tr}(I_{ab}) = 6 \frac{MR^2}{5} = \frac{2}{5} MR^2 \epsilon$.

Therefore in the quadrupole formula: $I_2 \sim \epsilon MR^2$

and: $\ddot{I}_2 \sim \frac{\epsilon MR^2}{P^2} = \epsilon MR^2 f_{\text{rot}}^2 = \epsilon MR^2 \frac{1}{P^2}$

$P^2 \rightarrow$ period $P = \frac{1}{f_{\text{rot}}}$

hence $h \sim \frac{G}{rc^4} \epsilon MR^2 f_{\text{rot}}^2$ which is off by numerical factors from (#2).
 \sim moment of inertia of sphere



$$\frac{Mv^2}{R} = \frac{GM^2}{(2R)^2} \rightarrow v^2 = \frac{GM}{4R} = \Omega^2 R^2$$

$$\rightarrow \Omega^2 = \frac{GM}{4R^3} = \frac{2GM}{(2R)^3}$$

So if we put $d \equiv 2R$ and $M_{\text{TOT}} = 2M$, we get:

$$\Omega^2 = \frac{GM_{\text{TOT}}}{d^3} \quad (\#3)$$

The trajectory of each object is:

$$\textcircled{1} \begin{cases} x_1(t) = R \cos(\Omega t) \\ y_1(t) = R \sin(\Omega t) \\ z_1(t) = 0 \end{cases}$$

$$\textcircled{2} \begin{cases} x_2(t) = -x_1(t) \\ y_2(t) = -y_1(t) \\ z_2(t) = 0 \end{cases}$$

$$I_{xx} = \int d^3x x^2 M [\delta(\vec{x} - \vec{x}_1(t)) + \delta(\vec{x} - \vec{x}_2(t))] = \text{integrated even under } x \rightarrow -x$$

$$= 2M \int d^3x x^2 \delta(x - x_1(t)) \delta(y - y_1(t)) \delta(z - z_1(t)) =$$

$$= 2MR^2 \cos^2(\Omega t)$$

$$I_{yy} = 2MR^2 \sin^2(\Omega t)$$

$$I_{xz} = I_{yz} = I_{zz} = 0$$

$$I_{xy} = 2MR^2 \sin(\Omega t) \cos(\Omega t) = MR^2 \sin(2\Omega t)$$

$$h \sim \frac{G}{c^4 r} \ddot{I}_2 \sim \frac{G}{c^4 r} \ddot{I}_{ij}$$

$$\ddot{I}_{xx} = -4MR^2\Omega^2 \cos(2\Omega t)$$

$$\ddot{I}_{yy} = 4MR^2\Omega^2 \cos(2\Omega t)$$

$$\ddot{I}_{xy} = -4MR^2\Omega^2 \sin(2\Omega t)$$

$$\Rightarrow 2\Omega = \omega_{GW} = 2\pi f_{GW} \Rightarrow \Omega = \pi f_{GW}$$

$$\text{then } h \sim \frac{G}{c^4 r} 4MR^2\Omega^2 \stackrel{\uparrow}{=} \frac{4GM\Omega^2}{c^4 r} \left(\frac{GM}{4\Omega^2}\right)^{2/3} = \frac{2^{2/3}}{c^4 r} (GM)^{5/3} \Omega^{2/3}$$

$$= \frac{(2\pi)^{2/3} (GM)^{5/3}}{c^4 r} f_{GW}^{2/3} \quad \begin{matrix} \text{(#3): } R^3 = \frac{GM}{4\Omega^2} \\ \text{(#4)} \end{matrix}$$

$$\Rightarrow h \propto M^{5/3} f_{GW}^{2/3}$$

This is correct, by comparison with Maggiore (4.3)

$$h_{+,x} \sim \frac{4}{r} \left(\frac{GM_c}{c^2}\right)^{5/3} \left(\frac{\pi f_{GW}}{c}\right)^{2/3}$$

$$\text{with } M_c = \frac{(M_1 M_2)^{3/5}}{(M_1 + M_2)^{1/5}} \stackrel{M_1=M_2=M}{=} \frac{M^{6/5}}{2^{1/5} M^{1/5}} = \frac{M}{2^{1/5}}$$

$$= \frac{4}{r} \frac{G^{5/3} \pi^{2/3} (M/2^{1/5})^{5/3} f_{GW}^{2/3}}{c^{10/3} c^{2/3}} =$$

$$= \frac{4}{r} \frac{G^{5/3} \pi^{2/3} M^{5/3} f_{GW}^{2/3}}{2^{1/3} c^4} =$$

$$= 2 \frac{(2\pi)^{2/3} (GM)^{5/3}}{c^4 r} f_{GW}^{2/3}$$

note that in our (#4) we are off by a factor of 2 w.r.t. Maggiore since we didn't include that factor in $h \sim \frac{2G\ddot{I}_2}{c^4 r}$

$$\text{let } f_{GW} = 100 \text{ Hz.}$$

$$\text{If } M = 1.4 M_\odot \text{ then } h \sim 110 \left(\frac{1 \text{ m}}{r}\right) \Rightarrow \text{to have } 10^{-21} = h \text{ we need } r \sim 10^{23} \text{ m} \cong$$

$$\cong 3.5 \text{ Mpc} \checkmark$$

$$\text{If } M = 10 M_\odot \text{ then } h \sim 3 \times 10^3 \left(\frac{1 \text{ m}}{r}\right) \Rightarrow r \sim 3 \times 10^{24} \text{ m} \sim 90 \text{ Mpc} \checkmark$$

$$\text{let } f_{GW} = 10^{-3} \text{ Hz and } M = 10^6 M_\odot, \text{ then } h \sim 30 \times 10^7 \left(\frac{1 \text{ m}}{r}\right) \checkmark$$

$$\Rightarrow r \sim 30 \times 10^{28} \text{ m} \cong 9400 \text{ Gpc} \checkmark$$