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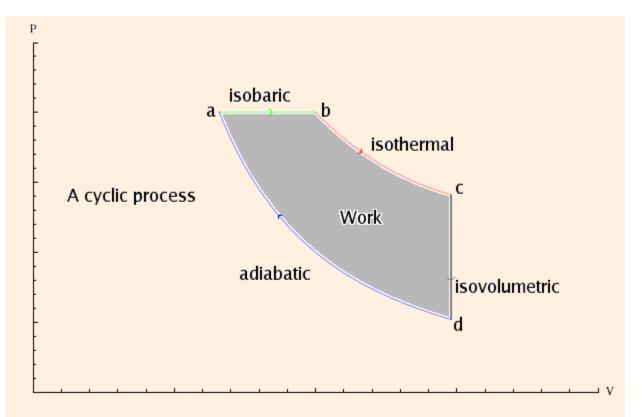
# Thermodynamics

- 1. Thermodynamic processes can be:
  - isothermal processes,  $\Delta T = 0$  (so P ~ 1 / V);
  - **isobaric processes**,  $\Delta P = 0$  (so T ~ V);
  - $\circ$  isovolumetric or isochoric processes,  $\Delta V = 0$  (so T ~ P);
  - adiabatic processes,  $\Delta Q = 0$  (so  $P \sim 1 / V^{\gamma}$ );
  - cyclic processes, *all* state variables (P, V, T, E, S) return to their original values after each cycle.

(Throughout, we will assume the processes involve an ideal gas with constant n.)

In a cyclic process, the state variables all return to their initial values after one cycle.

2. Thermodynamical systems are often described using **PV diagrams**, with pressure plotted on the vertical axis and volume plotted on the horizontal axis. In such a diagram, the area under a curve is easily related to work:



Assuming this PV diagram describes a process involving an ideal gas, we can deduce the following:

$$as a \rightarrow b \quad P_a = P_b \qquad \qquad \Delta E_{a \rightarrow b} = n c_v (T_b - T_a) \qquad \Delta Q_{a \rightarrow b} = n c_p (T_b - T_a) \qquad W_{a \rightarrow b} = -P_a (P_b - P_b) = -$$

at b	$T_b = P_b V_b / (n R)$	$T_b > T_a$	$\Delta Q_{a \rightarrow b} > 0$	$W_{a \rightarrow b} < 0$
as b→c	$T_b = T_c$	$\Delta E_{b \to c} = 0$	$\Delta Q_{b \to c} = -W_{b \to c}$	$W_{b \rightarrow c} = -n R$
at c	$T_{c} = P_{c} V_{c} / (n R)$		$\Delta Q_{b \rightarrow c} > 0$	$W_{b \rightarrow c} < 0$
as c→d	$V_c = V_d$	$\Delta E_{c \to d} = n c_v (T_d - T_c)$	$\Delta Q_{c \to d} = n c_v (T_d - T_c)$	$W_{c \rightarrow d} = 0$
at d	$T_d = P_d V_d / (n R)$	$T_d < T_c$	$\Delta Q_{c \rightarrow d} < 0$	
as d→a	$P_{d}V_{d}^{c_{p}/c_{v}} = P_{a}V_{a}^{c_{p}/c_{v}}$	$\Delta E_{d \to a} = n c_v (T_a - T_d)$	$\Delta Q_{d \to a} = 0$	$W_{d \rightarrow a} = n c_v$
at a	$T_a = P_a V_a / (n R)$	$T_a > T_d$		$W_{d \rightarrow a} > 0$

In addition, we know that  $\Delta E_{a \to b} + \Delta E_{c \to d} + \Delta E_{d \to a} = 0$ , but in this case it only tells us that  $T_b = T_c$ .

From this we can compute the total heat added during the cycle:

$$n c_{p} (T_{b} - T_{a}) + n R T_{b} ln (V_{c} / V_{b})$$

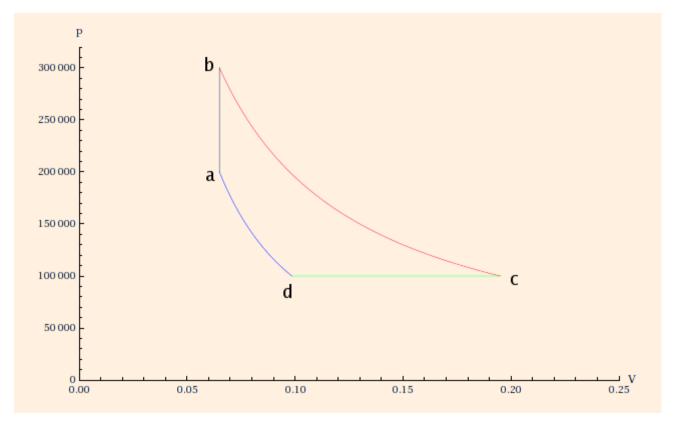
and the total work done by the gas:

$$P_{a} (V_{b} - V_{a}) + n R T_{b} ln (V_{c} / V_{b}) - n c_{v} (T_{a} - T_{d}),$$

corresponding to the shaded area in the PV diagram.

Note that heat enters this "engine" in steps  $a \rightarrow b$  and  $b \rightarrow c$ , and exits it in step  $c \rightarrow d$ ; the total work done by the engine is positive. If the cycle were operated in reverse, it would be a "refrigerator", taking heat from a cooler environment during step  $d \rightarrow c$  and exhausting it to a warmer environment from  $c \rightarrow a$ ; the total work done by the refrigerator is negative. The meaning of this is that it requires external work to move heat from a cooler to a warmer place.

3. To see how this information is applied to a problem, consider the following thermodynamic cycle for n = 4 moles of a monatomic ideal gas:



- 1. from a to b, the system undergoes an isovolumetric increase in pressure;
- 2. from b to c, the system undergoes an isothermal expansion;
- 3. from c to d, the system undergoes an isobaric compression;
- 4. from d to a, the system undergoes an adiabatic compression.

Suppose we are given  $P_a = 200,000 Pa$ ,  $P_b = 300,000 Pa$ ,  $P_c = 100,000 Pa$  and  $V_a = 65 L$ .

We know that  $P_d = P_c$ ,  $V_b = V_a$ , and  $T_b = T_c$ . We can use the ideal gas law to compute the temperatures at points a and b from the pressure and volumes at those points: 390.907 K and 586.36 K, respectively. From the latter we can compute the volume at point c, which is 195 L.

We can use the adiabatic equation for an ideal gas:

$$P_d V_d^{\gamma} = P_a V_a^{\gamma}$$

to compute  $V_d = 98.5216$  L. Finally, we can use the ideal gas law to find that  $T_d = 296.252$  K.

Since b to c is an isothermal expansion, the <u>first law</u> tells us that  $\Delta Q_{b\to c} = -\Delta W_{b\to c}$ . Using the ideal gas law, we find

$$\Delta W_{b\to c} = -\int_{b}^{c} P \, dV$$
  
= - n R T<sub>b</sub>  $\int_{b}^{c} dV / V$   
= - n R T<sub>b</sub> ln (V<sub>c</sub> / V<sub>b</sub>) = -21,422.9 J.

(Note the sign: the gas does external work.)

Using the equations for isovolumetric and isobaric processes, we have

$$\Delta Q_{a\to b} = n c_v (T_b - T_a) \qquad \Delta Q_{b\to c} = n R T_b \ln (V_c / V_b) \qquad \Delta Q_{c\to d} = n c_p (T_d - T_c)$$
  
= 9750 J = 21,422.9 J =-24,119.6 J

Finally, consistent with the fact that  $\Delta E = 0$  for a cycle, we compute

$$\Delta W_{a \to b} = 0 \quad \Delta W_{b \to c} = -n R T_b \ln (V_c / V_b) \qquad \Delta W_{c \to d} = P_c (V_c - V_d) \qquad \Delta W_{d \to a} = c_v (P_a V_a)$$
$$= -21,422.9 J \qquad = 9647.84 J \qquad = 4721$$

4. The efficiency of an engine is

$$\varepsilon = W / Q_h$$
$$= (Q_h - Q_c) / Q_h$$
$$= 1 - Q_c / Q_h.$$

Here, energy is taken in as  $Q_h$ , work W is done by the engine, and the waste heat is discharged as  $Q_c$ .

In the example above,  $Q_{h} = 31,172.9 \text{ J}$ , W = 7053.33 J,  $Q_{c} = 24,119.6 \text{ J}$  and  $\varepsilon = 22.6265\%$ .

This calculation obscures some interesting facts:

- o for this cycle, as the number of <u>degrees of freedom</u> of the gas χ→∞ (with all other values unchanged), ε→0 as 1/χ (more heat must be removed during isobaric cooling to lower the temperature the same amount, because more of the heat comes from non-translational degrees of freedom which do not affect temperature);
- ε does not depend on n; increasing n will only lower the temperatures (via the ideal gas law; with more molecules, less energy is available per molecule);
- while the efficiency is a complicated function of the given values, it is turns out that, holding all other values constant, increasing  $P_b$  or decreasing  $P_c$  will increase  $\varepsilon$ , while the value of  $V_a$  does not alter  $\varepsilon$  at all and the chosen value of  $P_a$  is almost optimal.

Of course, for another cycle, the results can be very different.

For an air conditioner, **heat pump** in air conditioning mode, or refrigerator,  $\varepsilon = Q_{\text{transferred}} / W_{\text{required}}$ . The efficiency of a refrigerator can be greater than 1, since

$$\varepsilon = Q_c / (Q_h - Q_c)$$

$$= 1 / (Q_h / Q_c - 1),$$

where  $Q_c$  is the heat removed from the cooler environment and  $Q_h$  is the heat exhausted into the warmer environment. Note that  $Q_h$  must be greater than  $Q_c$ .

5. We often consider a cycle operating between two **heat reservoirs** (of infinite <u>heat capacity</u>), one at temperature  $T_{h(ot)}$  and the other at temperature  $T_{c(old)}$ . For such a device,  $\Delta S$  includes the engine itself *and* the reservoirs. Since the engine operates in a cycle, its  $\Delta S$  is 0, so for isothermal transfers,

$$\Delta S = -\Delta Q_h / T_h + \Delta Q_c / T_c.$$

In general,  $\Delta S = \int dQ / T$ .

For the example above,  $\Delta S_{b\to c} = 36.5355 \text{ J/K}$ , and of course  $\Delta S_{d\to a} = 0$ . To compute  $\Delta S_{a\to b}$  and  $\Delta S_{c\to d}$ , we use the ideal gas law to express T as a function of P and V:

$$\Delta S_{a \to b} = \int n c_v dT / T$$
  
=  $\int n c_v (V dP / (n R)) / (P V / (n R))$   
=  $n c_v \ln (P_b / P_a) = 20.2262 J/K$ 

and

$$\Delta S_{c \to d} = \int n c_p dT / T$$
  
=  $\int n c_p (P dV / (n R)) / (P V / (n R))$   
=  $n c_p \ln (V_d / V_c) = -56.7617 J/K$ 

The changes in entropy of the reservoirs are of course dependent on their temperatures. Assuming that the isobaric compression lost heat to a reservoir at room temperature ( $< T_d$ ), and that the isochoric and isothermal processes gained heat from a reservoir at 320 C ( $> T_b$ ),

$$\Delta S_{\text{cold reservoir}} = 24119.6 / 293.15 \text{ J/K} = 82.277 \text{ J/K} \text{ and}$$
  
 $\Delta S_{\text{hot reservoir}} = -31172.9 / 593.15 \text{ J/K} = -52.555 \text{ J/K},$ 

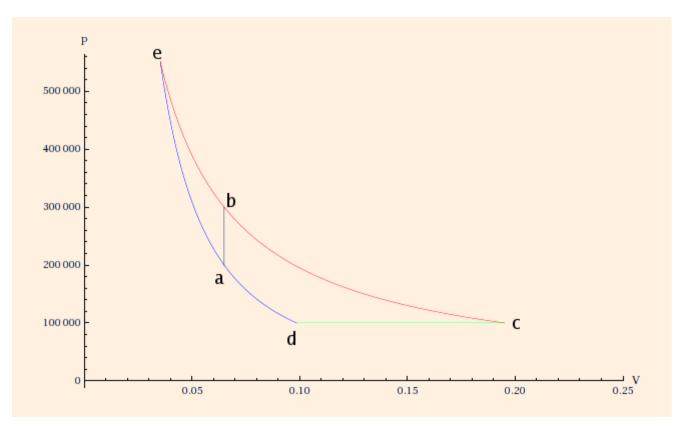
so that

$$\Delta S_{reservoirs} = 29.722 \text{ J/K},$$

which is greater than zero, as required by the second law of thermodynamics.

If we did not know T as a function of P and V, it would be necessary to connect each pair of endpoints with a combination of adiabatic and isothermal processes, and compute the change in entropy using

### those new processes. For example:



Process a $\rightarrow$ e is an adiabatic process, and e $\rightarrow$ b is isothermal. P<sub>e</sub> = 551,135 Pa and V<sub>e</sub> = 35.3815 L, from

$$P_{a} V_{a}^{\gamma} = P_{e} V_{e}^{\gamma}$$
$$= n R T_{b} V_{e}^{\gamma-1}$$

This gives us (using the same equations as above)

$$\Delta Q_{a \rightarrow e} = 0$$
 and  
 $\Delta Q_{e \rightarrow b} = 11,859.9 \text{ J}.$ 

Since entropy is a state variable,

$$\Delta S_{a \to b} = \Delta S_{e \to b} = 20.2262 \text{ J/K},$$

as before. Either way, the entropy change *of the engine* is zero, because it is a cycle: all state variables, including entropy, end at the same state in which they began. Therefore  $\Delta S_{c \rightarrow d} = -56.7617 \text{ J/K}$ .

- 6. The **Carnot cycle** is the most efficient cyclic thermodynamic process conceivable:
  - 1. isothermal expansion, with  $\Delta Q = Q_h$  at  $T_h$ ;
  - 2. adiabatic expansion, with  $T_h \rightarrow T_c$ ;

- 3. isothermal compression, with  $\Delta Q = -Q_c$  at  $T_c$ ; and
- 4. adiabatic compression, with  $T_c \rightarrow T_h$ .

What makes it so is that each step of the Carnot cycle is **reversible**: all changes of state are infinitesimally close to equilibrium.

Reversible changes of state are infinitely long; all real changes of state are irreversible.

In isothermal processes, by definition the gas is in thermal equilibrium with the reservoir. An adiabatic process can be irreversible:

Consider a closed, thermally insulated volume with a partition in the middle, such that nearly all of the gas molecules are on one side of the partition; the other side is a nearly perfect vacuum. With removal of the partition, the gas adiabatically but irreversibly doubles in volume.

A reversible adiabatic process would be a change in volume by infinitesimal steps while the gas is thermally insulated.

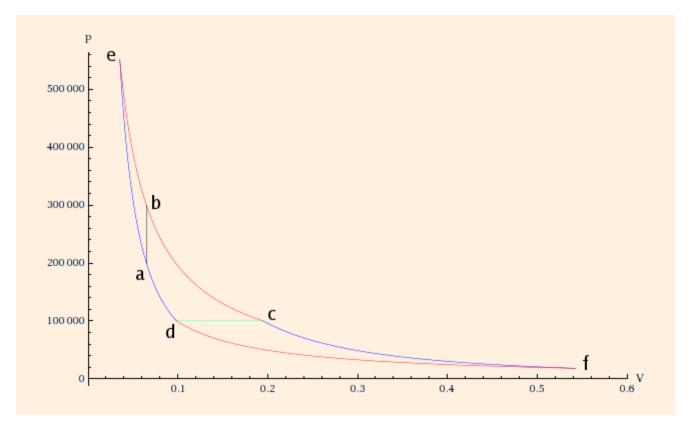
Since it is reversible, the total entropy change of the Carnot cycle reservoirs is zero. This gives us

$$0 = -Q_h / T_h + Q_c / T_c$$

or

$$Q_c / Q_h = T_c / T_h.$$

If we attempt to compute the entropy change for  $c \rightarrow d$  by finding a point f on the PV diagram such that  $c \rightarrow f$  is adiabatic and  $f \rightarrow d$  is isothermal, we find that we have constructed a Carnot cycle:



Hence the total entropy change is zero including the reservoirs, and its efficiency is

$$1 - T_d / T_b = 49.4761\%$$

The efficiency of a Carnot Refrigerator is  $T_c / (T_h - T_c)$ .

- 7. Thermodynamic cycles of practical interest include:
  - the **Diesel Engine**, consisting of adiabatic compression  $(a \rightarrow b)$ , isobaric heating  $(b \rightarrow c)$ , adiabatic expansion  $(c \rightarrow d)$  and isovolumetric cooling  $(d \rightarrow a)$ ;

$$\varepsilon = 1 - (T_d - T_a) / ((1 + 2 / \chi) (T_c - T_b))$$

• the **Otto Cycle**, consisting of adiabatic compression, isovolumetric heating, adiabatic expansion and isovolumetric cooling;

$$\varepsilon = 1 - (V_{small} / V_{large})^{(2 / \chi)}$$

• the **Stirling Engine**, consisting of alternating isothermal and isovolumetric processes.

$$\varepsilon = 1 / (1 + T_{lower} / |\Delta T| + \chi / (2 \ln (V_{large} / V_{small})))$$

In each case,  $\epsilon$  was computed for an ideal gas. Note that in each case, it is independent of n, and increases with decreasing  $\chi$ . This generalizes what we saw above: if we think of work as the result of increased temperature, less heat input is required to change the temperature of a gas with fewer degrees of freedom.

- 8. It is important to remember that these are *models* of real thermodynamic process. In actual physical processes,
  - gasses are *never* perfectly ideal;
  - n is *never* constant;
  - nothing has infinite heat capacity; and
  - no process is perfectly adiabatic (or, of course, reversible).

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