## Thermodynamics

1. Thermodynamic processes can be:

- isothermal processes, $\Delta \mathrm{T}=0$ (so $\mathrm{P} \sim 1 / \mathrm{V}$ );
- isobaric processes, $\Delta \mathrm{P}=0$ (so $\mathrm{T} \sim \mathrm{V}$ );
- isovolumetric or isochoric processes, $\Delta \mathrm{V}=0$ (so $\mathrm{T} \sim \mathrm{P}$ );
- adiabatic processes, $\Delta \mathrm{Q}=0$ (so $\mathrm{P} \sim 1 / \mathrm{V}^{\gamma}$ );
- cyclic processes, all state variables (P, V, T, E, S) return to their original values after each cycle. (Throughout, we will assume the processes involve an ideal gas with constant n.)

In a cyclic process, the state variables all return to their initial values after one cycle.
2. Thermodynamical systems are often described using PV diagrams, with pressure plotted on the vertical axis and volume plotted on the horizontal axis. In such a diagram, the area under a curve is easily related to work:


Assuming this PV diagram describes a process involving an ideal gas, we can deduce the following:

| as $a \rightarrow b$ | $P_{a}=P_{b}$ | $\Delta E_{a \rightarrow b}=n c_{v}\left(T_{b}-T_{a}\right)$ | $\Delta Q_{a \rightarrow b}=n_{p}\left(T_{b}-T_{a}\right)$ |
| :--- | :--- | :--- | :--- |$W_{a \rightarrow b}=-P_{a}($


| at b | $\mathrm{T}_{\mathrm{b}}=\mathrm{P}_{\mathrm{b}} \mathrm{V}_{\mathrm{b}} /(\mathrm{nR})$ | $\mathrm{T}_{\mathrm{b}}>\mathrm{T}_{\mathrm{a}}$ | $\Delta \mathrm{Q}_{\mathrm{a} \rightarrow \mathrm{b}}>0$ | $\mathrm{W}_{\mathrm{a} \rightarrow \mathrm{b}}<0$ |
| :---: | :---: | :---: | :---: | :---: |
| as $\mathrm{b} \rightarrow \mathrm{c}$ | $\mathrm{T}_{\mathrm{b}}=\mathrm{T}_{\mathrm{c}}$ | $\Delta \mathrm{E}_{\mathrm{b} \rightarrow \mathrm{c}}=0$ | $\Delta \mathrm{Q}_{\mathrm{b} \rightarrow \mathrm{c}}=-\mathrm{W}_{\mathrm{b} \rightarrow \mathrm{c}}$ | $\mathrm{W}_{\mathrm{b} \rightarrow \mathrm{c}}=-\mathrm{nR}$ |
| at c | $\mathrm{T}_{\mathrm{c}}=\mathrm{P}_{\mathrm{c}} \mathrm{V}_{\mathrm{c}} /(\mathrm{nR})$ |  | $\Delta \mathrm{Q}_{\mathrm{b} \rightarrow \mathrm{c}}>0$ | $\mathrm{W}_{\mathrm{b} \rightarrow \mathrm{c}}<0$ |
| as $\mathrm{c} \rightarrow \mathrm{d}$ | $\mathrm{V}_{\mathrm{c}}=\mathrm{V}_{\mathrm{d}}$ | $\Delta \mathrm{E}_{\mathrm{c} \rightarrow \mathrm{d}}=\mathrm{nc}_{\mathrm{v}}\left(\mathrm{T}_{\mathrm{d}}-\mathrm{T}_{\mathrm{c}}\right)$ | $\Delta \mathrm{Q}_{\mathrm{c} \rightarrow \mathrm{d}}=\mathrm{nc}_{\mathrm{v}}\left(\mathrm{T}_{\mathrm{d}}-\mathrm{T}_{\mathrm{c}}\right)$ | $\mathrm{W}_{\mathrm{c} \rightarrow \mathrm{d}}=0$ |
| at d | $\mathrm{T}_{\mathrm{d}}=\mathrm{P}_{\mathrm{d}} \mathrm{V}_{\mathrm{d}} /(\mathrm{nR})$ | $\mathrm{T}_{\mathrm{d}}<\mathrm{T}_{\mathrm{c}}$ | $\Delta \mathrm{Q}_{\mathrm{c} \rightarrow \mathrm{d}}<0$ |  |
| as $\mathrm{d} \rightarrow \mathrm{a}$ | $P_{d} V_{d}^{c_{p} / c_{v}=} P_{a} V_{a}^{c_{p} / c_{v}}$ | $\Delta \mathrm{E}_{\mathrm{d} \rightarrow \mathrm{a}}=\mathrm{nc}_{\mathrm{v}}\left(\mathrm{~T}_{\mathrm{a}}-\mathrm{T}_{\mathrm{d}}\right)$ | $\Delta Q_{d \rightarrow a}=0$ | $\mathrm{W}_{\mathrm{d} \rightarrow \mathrm{a}}=\mathrm{nc}_{\mathrm{v}}{ }^{\prime}$ |
| at a | $\mathrm{T}_{\mathrm{a}}=\mathrm{P}_{\mathrm{a}} \mathrm{V}_{\mathrm{a}} /(\mathrm{nR})$ | $\mathrm{T}_{\mathrm{a}}>\mathrm{T}_{\mathrm{d}}$ |  | $\mathrm{W}_{\mathrm{d} \rightarrow \mathrm{a}}>0$ |

In addition, we know that $\Delta \mathrm{E}_{\mathrm{a} \rightarrow \mathrm{b}}+\Delta \mathrm{E}_{\mathrm{c} \rightarrow \mathrm{d}}+\Delta \mathrm{E}_{\mathrm{d} \rightarrow \mathrm{a}}=0$, but in this case it only tells us that $\mathrm{T}_{\mathrm{b}}=\mathrm{T}_{\mathrm{c}}$.
From this we can compute the total heat added during the cycle:

$$
n c_{p}\left(T_{b}-T_{a}\right)+n R T_{b} \ln \left(V_{c} / V_{b}\right)
$$

and the total work done by the gas:

$$
\mathrm{P}_{\mathrm{a}}\left(\mathrm{~V}_{\mathrm{b}}-\mathrm{V}_{\mathrm{a}}\right)+\mathrm{nR} \mathrm{~T}_{\mathrm{b}} \ln \left(\mathrm{~V}_{\mathrm{c}} / \mathrm{V}_{\mathrm{b}}\right)-\mathrm{nc}_{\mathrm{v}}\left(\mathrm{~T}_{\mathrm{a}}-\mathrm{T}_{\mathrm{d}}\right)
$$

corresponding to the shaded area in the PV diagram.
Note that heat enters this "engine" in steps $a \rightarrow b$ and $b \rightarrow c$, and exits it in step $c \rightarrow d$; the total work done by the engine is positive. If the cycle were operated in reverse, it would be a "refrigerator", taking heat from a cooler environment during step $\mathrm{d} \rightarrow \mathrm{c}$ and exhausting it to a warmer environment from $\mathrm{c} \rightarrow \mathrm{a}$; the total work done by the refrigerator is negative. The meaning of this is that it requires external work to move heat from a cooler to a warmer place.
3. To see how this information is applied to a problem, consider the following thermodynamic cycle for n $=4$ moles of a monatomic ideal gas:


1. from $a$ to $b$, the system undergoes an isovolumetric increase in pressure;
2. from $b$ to $c$, the system undergoes an isothermal expansion;
3. from c to d , the system undergoes an isobaric compression;
4. from d to a , the system undergoes an adiabatic compression.

Suppose we are given $\mathrm{P}_{\mathrm{a}}=200,000 \mathrm{~Pa}, \mathrm{P}_{\mathrm{b}}=300,000 \mathrm{~Pa}, \mathrm{P}_{\mathrm{c}}=100,000 \mathrm{~Pa}$ and $\mathrm{V}_{\mathrm{a}}=65 \mathrm{~L}$.
We know that $\mathrm{P}_{\mathrm{d}}=\mathrm{P}_{\mathrm{c}}, \mathrm{V}_{\mathrm{b}}=\mathrm{V}_{\mathrm{a}}$, and $\mathrm{T}_{\mathrm{b}}=\mathrm{T}_{\mathrm{c}}$. We can use the ideal gas law to compute the temperatures at points $a$ and $b$ from the pressure and volumes at those points: 390.907 K and 586.36 K , respectively. From the latter we can compute the volume at point c, which is 195 L .

We can use the adiabatic equation for an ideal gas:

$$
\mathrm{P}_{\mathrm{d}} \mathrm{~V}_{\mathrm{d}}^{\gamma}=\mathrm{P}_{\mathrm{a}} \mathrm{~V}_{\mathrm{a}}^{\gamma},
$$

to compute $\mathrm{V}_{\mathrm{d}}=98.5216 \mathrm{~L}$. Finally, we can use the ideal gas law to find that $\mathrm{T}_{\mathrm{d}}=296.252 \mathrm{~K}$.
Since $b$ to $c$ is an isothermal expansion, the first law tells us that $\Delta \mathrm{Q}_{\mathrm{b} \rightarrow \mathrm{c}}=-\Delta \mathrm{W}_{\mathrm{b} \rightarrow \mathrm{c}}$. Using the ideal gas law, we find

$$
\begin{aligned}
\Delta \mathrm{W}_{\mathrm{b} \rightarrow \mathrm{c}} & =-\int_{\mathrm{b}}^{\mathrm{c}} \mathrm{P} d V \\
& =-\mathrm{nR} \mathrm{~T}_{\mathrm{b}} \int_{\mathrm{b}}^{\mathrm{c}} \mathrm{dV} / \mathrm{V} \\
& =-\mathrm{nR} \mathrm{~T}_{\mathrm{b}} \ln \left(\mathrm{~V}_{\mathrm{c}} / \mathrm{V}_{\mathrm{b}}\right)=-21,422.9 \mathrm{~J}
\end{aligned}
$$

(Note the sign: the gas does external work.)
Using the equations for isovolumetric and isobaric processes, we have

$$
\begin{array}{rlrl}
\Delta \mathrm{Q}_{\mathrm{a} \rightarrow \mathrm{~b}}=\mathrm{nc}_{\mathrm{v}}\left(\mathrm{~T}_{\mathrm{b}}-\mathrm{T}_{\mathrm{a}}\right) & \Delta \mathrm{Q}_{\mathrm{b} \rightarrow \mathrm{c}}=\mathrm{n} \mathrm{R} \mathrm{~T}_{\mathrm{b}} \ln \left(\mathrm{~V}_{\mathrm{c}} / \mathrm{V}_{\mathrm{b}}\right) & \Delta \mathrm{Q}_{\mathrm{c} \rightarrow \mathrm{~d}} & =\mathrm{nc}_{\mathrm{p}}\left(\mathrm{~T}_{\mathrm{d}}-\mathrm{T}_{\mathrm{c}}\right) \\
=9750 \mathrm{~J} & =21,422.9 \mathrm{~J} & =-24,119.6 \mathrm{~J}
\end{array}
$$

Finally, consistent with the fact that $\Delta \mathrm{E}=0$ for a cycle, we compute

$$
\begin{array}{rlrl}
\Delta \mathrm{W}_{\mathrm{a} \rightarrow \mathrm{~b}}=0 \quad \Delta \mathrm{~W}_{\mathrm{b} \rightarrow \mathrm{c}}=- & -\mathrm{nR} \mathrm{~T}_{\mathrm{b}} \ln \left(\mathrm{~V}_{\mathrm{c}} / \mathrm{V}_{\mathrm{b}}\right) & \Delta \mathrm{W}_{\mathrm{c} \rightarrow \mathrm{~d}} & =\mathrm{P}_{\mathrm{c}}\left(\mathrm{~V}_{\mathrm{c}}-\mathrm{V}_{\mathrm{d}}\right) \\
& =-21,422.9 \mathrm{~J} & =9647.84 \mathrm{~J} & \mathrm{~W}_{\mathrm{d} \rightarrow \mathrm{a}}=\mathrm{c}_{\mathrm{v}}\left(\mathrm{P}_{\mathrm{a}} \mathrm{~V}_{\mathrm{a}}\right. \\
& =4721
\end{array}
$$

4. The efficiency of an engine is

$$
\begin{aligned}
\varepsilon=\mathrm{W} & / \mathrm{Q}_{\mathrm{h}} \\
& =\left(\mathrm{Q}_{\mathrm{h}}-\mathrm{Q}_{\mathrm{c}}\right) / \mathrm{Q}_{\mathrm{h}} \\
& =1-\mathrm{Q}_{\mathrm{c}} / \mathrm{Q}_{\mathrm{h}} .
\end{aligned}
$$

Here, energy is taken in as $Q_{h}$, work $W$ is done by the engine, and the waste heat is discharged as $\mathrm{Q}_{\mathrm{c}}$.

In the example above, $\mathrm{Q}_{\mathrm{h}}=31,172.9 \mathrm{~J}, \mathrm{~W}=7053.33 \mathrm{~J}, \mathrm{Q}_{\mathrm{c}}=24,119.6 \mathrm{~J}$ and $\varepsilon=22.6265 \%$.
This calculation obscures some interesting facts:

- for this cycle, as the number of degrees of freedom of the gas $\chi \rightarrow \infty$ (with all other values unchanged), $\varepsilon \rightarrow 0$ as $1 / \chi$ (more heat must be removed during isobaric cooling to lower the temperature the same amount, because more of the heat comes from non-translational degrees of freedom which do not affect temperature);
$\circ \varepsilon$ does not depend on n ; increasing n will only lower the temperatures (via the ideal gas law; with more molecules, less energy is available per molecule);
- while the efficiency is a complicated function of the given values, it is turns out that, holding all other values constant, increasing $\mathrm{P}_{\mathrm{b}}$ or decreasing $\mathrm{P}_{\mathrm{c}}$ will increase $\varepsilon$, while the value of $\mathrm{V}_{\mathrm{a}}$ does not alter $\varepsilon$ at all and the chosen value of $\mathrm{P}_{\mathrm{a}}$ is almost optimal.

Of course, for another cycle, the results can be very different.
For an air conditioner, heat pump in air conditioning mode, or refrigerator, $\varepsilon=\mathrm{Q}_{\text {transferred }} / \mathrm{W}_{\text {required }}$. The efficiency of a refrigerator can be greater than 1 , since

$$
\varepsilon=\mathrm{Q}_{\mathrm{c}} /\left(\mathrm{Q}_{\mathrm{h}}-\mathrm{Q}_{\mathrm{c}}\right)
$$

$$
=1 /\left(\mathrm{Q}_{\mathrm{h}} / \mathrm{Q}_{\mathrm{c}}-1\right)
$$

where $Q_{c}$ is the heat removed from the cooler environment and $Q_{h}$ is the heat exhausted into the warmer environment. Note that $\mathrm{Q}_{\mathrm{h}}$ must be greater than $\mathrm{Q}_{\mathrm{c}}$.
5. We often consider a cycle operating between two heat reservoirs (of infinite heat capacity), one at temperature $\mathrm{T}_{\mathrm{h}(\mathrm{ot})}$ and the other at temperature $\mathrm{T}_{\mathrm{c}(\mathrm{old})}$. For such a device, $\underline{\Delta \mathrm{S}}$ includes the engine itself and the reservoirs. Since the engine operates in a cycle, its $\underline{\Delta S}$ is 0 , so for isothermal transfers,

$$
\Delta S=-\Delta Q_{h} / T_{h}+\Delta Q_{c} / T_{c}
$$

In general, $\Delta \mathrm{S}=\int \mathrm{dQ} / \mathrm{T}$.
For the example above, $\Delta \mathrm{S}_{\mathrm{b} \rightarrow \mathrm{c}}=36.5355 \mathrm{~J} / \mathrm{K}$, and of course $\Delta \mathrm{S}_{\mathrm{d} \rightarrow \mathrm{a}}=0$. To compute $\Delta \mathrm{S}_{\mathrm{a} \rightarrow \mathrm{b}}$ and $\Delta \mathrm{S}_{\mathrm{c} \rightarrow \mathrm{d}}$, we use the ideal gas law to express T as a function of P and V :

$$
\begin{aligned}
\Delta \mathrm{S}_{\mathrm{a} \rightarrow \mathrm{~b}} & =\int \mathrm{nc}_{\mathrm{v}} \mathrm{dT} / \mathrm{T} \\
& =\int \mathrm{nc}_{\mathrm{v}}(\mathrm{~V} \mathrm{dP} /(\mathrm{nR})) /(\mathrm{PV} /(\mathrm{nR})) \\
& =\mathrm{nc}_{\mathrm{v}} \ln \left(\mathrm{P}_{\mathrm{b}} / \mathrm{P}_{\mathrm{a}}\right)=20.2262 \mathrm{~J} / \mathrm{K}
\end{aligned}
$$

and

$$
\begin{aligned}
\Delta \mathrm{S}_{\mathrm{c} \rightarrow \mathrm{~d}} & =\int \mathrm{nc}_{\mathrm{p}} \mathrm{dT} / \mathrm{T} \\
& =\int \mathrm{n} \mathrm{c}_{\mathrm{p}}(\mathrm{PdV} /(\mathrm{nR})) /(\mathrm{PV} /(\mathrm{nR})) \\
& =\mathrm{n} \mathrm{c}_{\mathrm{p}} \ln \left(\mathrm{~V}_{\mathrm{d}} / \mathrm{V}_{\mathrm{c}}\right)=-56.7617 \mathrm{~J} / \mathrm{K}
\end{aligned}
$$

The changes in entropy of the reservoirs are of course dependent on their temperatures. Assuming that the isobaric compression lost heat to a reservoir at room temperature $\left(<T_{d}\right)$, and that the isochoric and isothermal processes gained heat from a reservoir at $320 \mathrm{C}\left(>\mathrm{T}_{\mathrm{b}}\right)$,

$$
\begin{aligned}
& \Delta \mathrm{S}_{\text {cold reservoir }}=24119.6 / 293.15 \mathrm{~J} / \mathrm{K}=82.277 \mathrm{~J} / \mathrm{K} \text { and } \\
& \Delta \mathrm{S}_{\text {hot reservoir }}=-31172.9 / 593.15 \mathrm{~J} / \mathrm{K}=-52.555 \mathrm{~J} / \mathrm{K},
\end{aligned}
$$

so that

$$
\Delta \mathrm{S}_{\text {reservoirs }}=29.722 \mathrm{~J} / \mathrm{K}
$$

which is greater than zero, as required by the second law of thermodynamics.
If we did not know T as a function of P and V , it would be necessary to connect each pair of endpoints with a combination of adiabatic and isothermal processes, and compute the change in entropy using
those new processes. For example:


Process $\mathrm{a} \rightarrow \mathrm{e}$ is an adiabatic process, and $\mathrm{e} \rightarrow \mathrm{b}$ is isothermal. $\mathrm{P}_{\mathrm{e}}=551,135 \mathrm{~Pa}$ and $\mathrm{V}_{\mathrm{e}}=35.3815 \mathrm{~L}$, from

$$
\begin{aligned}
\mathrm{P}_{\mathrm{a}} \mathrm{~V}_{\mathrm{a}}^{\gamma} & =\mathrm{P}_{\mathrm{e}} \mathrm{~V}_{\mathrm{e}}^{\gamma} \\
& =\mathrm{nR} \mathrm{~T}_{\mathrm{b}} \mathrm{~V}_{\mathrm{e}}^{\gamma-1}
\end{aligned}
$$

This gives us (using the same equations as above)

$$
\begin{aligned}
& \Delta \mathrm{Q}_{\mathrm{a} \rightarrow \mathrm{e}}=0 \text { and } \\
& \Delta \mathrm{Q}_{\mathrm{e} \rightarrow \mathrm{~b}}=11,859.9 \mathrm{~J} .
\end{aligned}
$$

Since entropy is a state variable,

$$
\Delta \mathrm{S}_{\mathrm{a} \rightarrow \mathrm{~b}}=\Delta \mathrm{S}_{\mathrm{e} \rightarrow \mathrm{~b}}=20.2262 \mathrm{~J} / \mathrm{K},
$$

as before. Either way, the entropy change of the engine is zero, because it is a cycle: all state variables, including entropy, end at the same state in which they began. Therefore $\Delta \mathrm{S}_{\mathrm{c} \rightarrow \mathrm{d}}=-56.7617 \mathrm{~J} / \mathrm{K}$.
6. The Carnot cycle is the most efficient cyclic thermodynamic process conceivable:

1. isothermal expansion, with $\Delta \mathrm{Q}=\mathrm{Q}_{\mathrm{h}}$ at $\mathrm{T}_{\mathrm{h}}$;
2. adiabatic expansion, with $\mathrm{T}_{\mathrm{h}} \rightarrow \mathrm{T}_{\mathrm{c}}$;
3. isothermal compression, with $\Delta \mathrm{Q}=-\mathrm{Q}_{\mathrm{c}}$ at $\mathrm{T}_{\mathrm{c}}$; and
4. adiabatic compression, with $\mathrm{T}_{\mathrm{c}} \rightarrow \mathrm{T}_{\mathrm{h}}$.

What makes it so is that each step of the Carnot cycle is reversible: all changes of state are infinitesimally close to equilibrium.

Reversible changes of state are infinitely long; all real changes of state are irreversible.
In isothermal processes, by definition the gas is in thermal equilibrium with the reservoir. An adiabatic process can be irreversible:

Consider a closed, thermally insulated volume with a partition in the middle, such that nearly all of the gas molecules are on one side of the partition; the other side is a nearly perfect vacuum. With removal of the partition, the gas adiabatically but irreversibly doubles in volume.

A reversible adiabatic process would be a change in volume by infinitesimal steps while the gas is thermally insulated.

Since it is reversible, the total entropy change of the Carnot cycle reservoirs is zero. This gives us

$$
0=-Q_{h} / T_{h}+Q_{c} / T_{c}
$$

or

$$
\mathrm{Q}_{\mathrm{c}} / \mathrm{Q}_{\mathrm{h}}=\mathrm{T}_{\mathrm{c}} / \mathrm{T}_{\mathrm{h}} .
$$

If we attempt to compute the entropy change for $\mathrm{c} \rightarrow \mathrm{d}$ by finding a point f on the PV diagram such that $\mathrm{c} \rightarrow \mathrm{f}$ is adiabatic and $\mathrm{f} \rightarrow \mathrm{d}$ is isothermal, we find that we have constructed a Carnot cycle:


Hence the total entropy change is zero including the reservoirs, and its efficiency is
$1-T_{d} / T_{b}=49.4761 \%$.
The efficiency of a Carnot Refrigerator is $T_{c} /\left(T_{h}-T_{c}\right)$.
7. Thermodynamic cycles of practical interest include:
$\circ$ the Diesel Engine, consisting of adiabatic compression $(a \rightarrow b)$, isobaric heating $(b \rightarrow c)$, adiabatic expansion $(c \rightarrow d)$ and isovolumetric cooling $(d \rightarrow a)$;

$$
\varepsilon=1-\left(T_{d}-T_{a}\right) /\left((1+2 / \chi)\left(T_{c}-T_{b}\right)\right)
$$

- the Otto Cycle, consisting of adiabatic compression, isovolumetric heating, adiabatic expansion and isovolumetric cooling;

$$
\varepsilon=1-\left(\mathrm{V}_{\text {small }} / \mathrm{V}_{\text {large }}\right)^{(2 / \chi)}
$$

$\circ$ the Stirling Engine, consisting of alternating isothermal and isovolumetric processes.

$$
\varepsilon=1 /\left(1+\mathrm{T}_{\text {lower }} /|\Delta \mathrm{T}|+\chi /\left(2 \ln \left(\mathrm{~V}_{\text {large }} / \mathrm{V}_{\text {small }}\right)\right)\right)
$$

In each case, $\varepsilon$ was computed for an ideal gas. Note that in each case, it is independent of n , and increases with decreasing $\chi$. This generalizes what we saw above: if we think of work as the result of increased temperature, less heat input is required to change the temperature of a gas with fewer degrees of freedom.
8. It is important to remember that these are models of real thermodynamic process. In actual physical processes,

- gasses are never perfectly ideal;
- n is never constant;
- nothing has infinite heat capacity; and
- no process is perfectly adiabatic (or, of course, reversible).
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