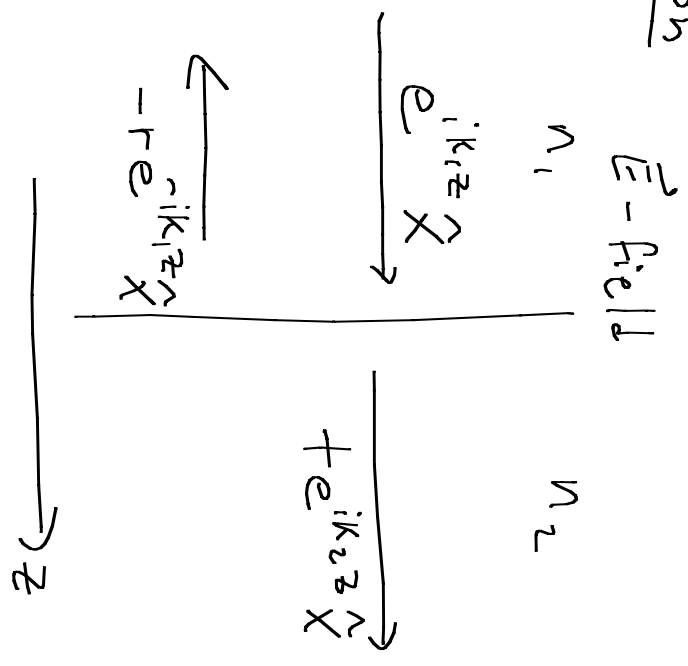
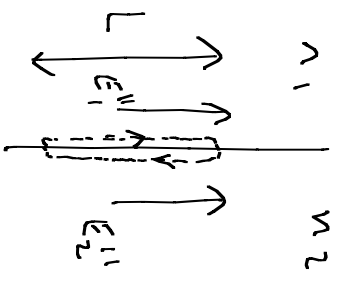


Reflection



Boundary
condition:



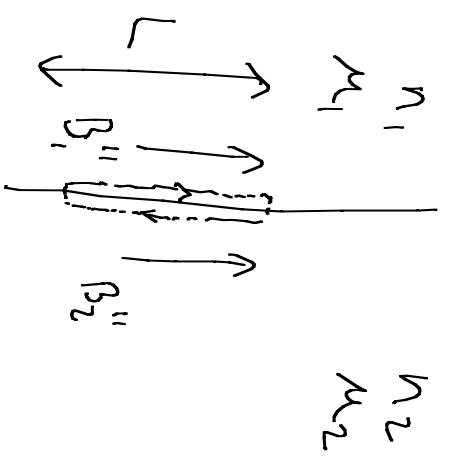
$$\oint \vec{E} \cdot d\vec{s} = -\frac{d\Phi_B}{dt}$$

$$E_1'' L - E_2'' L = 0$$

$$E_1'' = E_2''$$

we have 2 unknowns!
 → we need 2 B.C.'s!

B.C. for Magnetized Field



$$\oint \vec{B} \cdot d\vec{l} = \mu I + \mu \epsilon \frac{d\phi}{dt}$$

$$\oint \frac{\vec{B}}{\mu} \cdot d\vec{l} = 0$$

$$\frac{B_1''}{\mu_1} L - \frac{B_2''}{\mu_2} L = 0$$

$$\frac{B_1''}{\mu_1} = \frac{B_2''}{\mu_2}$$

$$(H_1'' = H_2'')$$

Plane wave \vec{B} Components

$$\vec{E} = E_0 e^{i(kz - \omega t)} \hat{x}$$

Faraday's Law: $\vec{\nabla} \times \vec{E} = -\frac{d\vec{B}}{dt}$

$$\begin{aligned} \vec{\nabla} \times \vec{E} &= \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{d}{dx} & \frac{d}{dy} & \frac{d}{dz} \\ E_0 e^{i(kz - \omega t)} & 0 & 0 \end{vmatrix} \\ &= 0 \hat{x} - (0 - ikE_0 e^{i(kz - \omega t)}) \hat{y} + 0 \hat{z} \\ &= ikE_0 e^{i(kz - \omega t)} \hat{y} \end{aligned}$$

$$\vec{B} = (B_x \hat{x} + B_y \hat{y} + B_z \hat{z}) e^{i(kz - \omega t)}$$

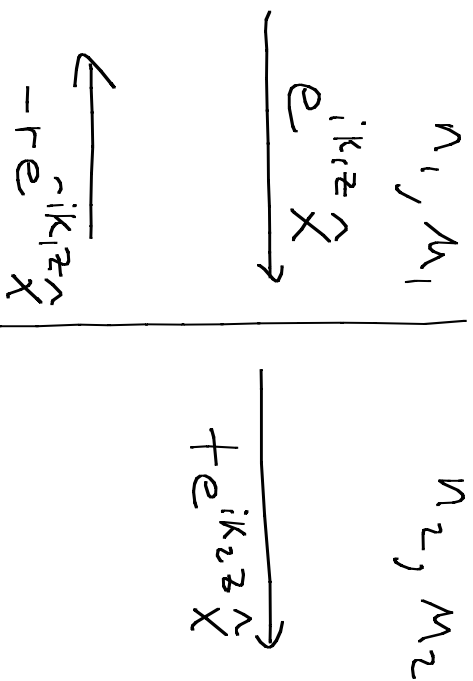
$$-\frac{d\vec{B}}{dt} = -(-i\omega (B_x \hat{x} + B_y \hat{y} + B_z \hat{z})) e^{i(kz - \omega t)}$$

$$\vec{\nabla} \times \vec{E} = -\frac{d\vec{B}}{dt} : \quad ikE_0 e^{i(kz - \omega t)} \hat{y} = i\omega B_y e^{i(kz - \omega t)} \hat{y}$$

$$B_y = \frac{k}{\omega} E_0 = \frac{E_0}{v} = \frac{nE_0}{c}$$

Imposing Boundary Conditions

\vec{E} -Field



BC's: ① $E_1'' = E_2''$ ② $\frac{B_1''}{\mu_1} = \frac{B_2''}{\mu_2}$ ($B'' = \frac{n}{c} E''$)

①: $e^{ik_1 z} - r e^{-ik_1 z} \Big|_{z=0} = + e^{ik_2 z} \Big|_{z=0} \rightarrow 1 - r = +$

②: $\frac{n_1}{\mu_1 c} e^{ik_1 z} - \frac{n_1}{\mu_1 c} r e^{-ik_1 z} \Big|_{z=0} = \frac{n_2}{\mu_2 c} + e^{ik_2 z} \Big|_{z=0} \rightarrow \frac{n_1}{\mu_1} - r \frac{n_1}{\mu_1} = \frac{n_2}{\mu_2} +$

$$\frac{n_1}{\mu_1} - r \frac{n_1}{\mu_1} = \frac{n_2}{\mu_2} (1 - r)$$

$$\frac{n_1}{\mu_1} = \frac{n_2}{\mu_2} - r \left(\frac{n_1}{\mu_1} + \frac{n_2}{\mu_2} \right)$$

$$r = \frac{\frac{n_2}{\mu_2} - \frac{n_1}{\mu_1}}{\frac{n_1}{\mu_1} + \frac{n_2}{\mu_2}}$$

We measure
E-Fields!

Intensity = $|E|^2$, not

$$R = |r|^2 =$$

$$\left(\frac{\frac{n_2}{\mu_2} - \frac{n_1}{\mu_1}}{\frac{n_1}{\mu_1} + \frac{n_2}{\mu_2}} \right)^2$$

$$\frac{\mu c}{n} = \frac{\mu}{\sqrt{\mu \epsilon}} = \sqrt{\frac{\mu}{\epsilon}}$$

"Intrinsic Impedance"

When $n_1 = n_2$,

$$R = \left(\frac{n_1 - n_2}{n_1 + n_2} \right)^2$$

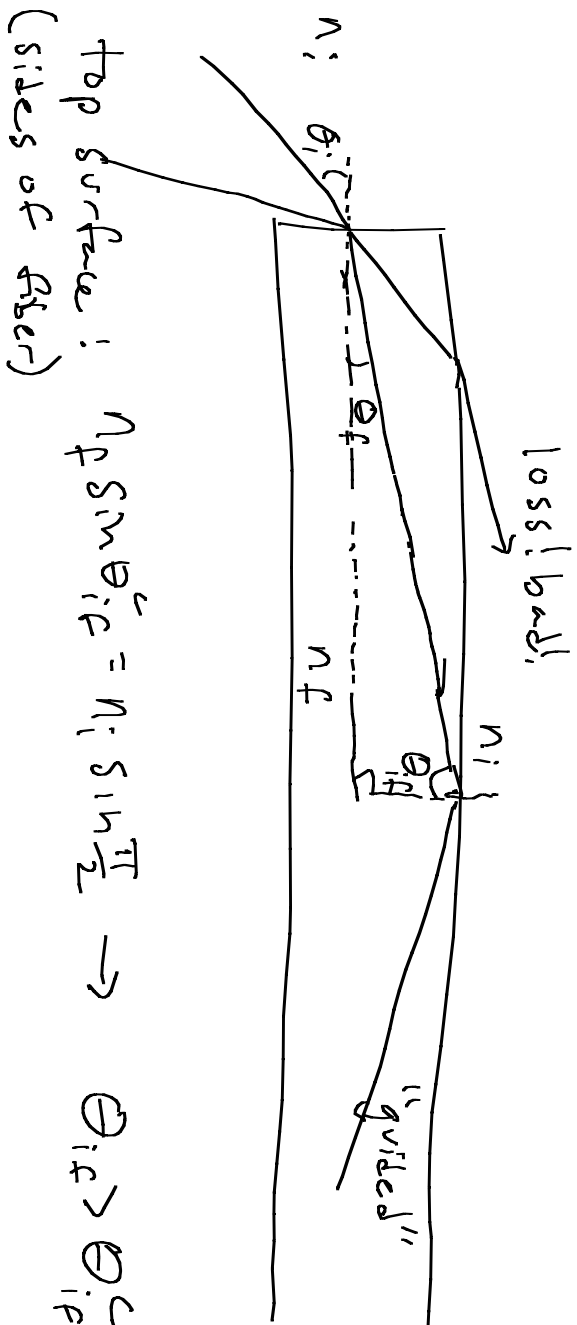
$$R + T = 1 \quad T = 1 - R$$

$$T = 1 - \left(\frac{n_1 - n_2}{n_1 + n_2} \right)^2 = \frac{(n_1 + n_2)^2}{(n_1 + n_2)^2} - \frac{(n_1 - n_2)^2}{(n_1 + n_2)^2}$$

$$= \frac{n_1^2 + n_2^2 + 2n_1n_2 - (n_1^2 + n_2^2 - 2n_1n_2)}{(n_1 + n_2)^2} = \frac{4n_1n_2}{(n_1 + n_2)^2}$$

Reflection is consequence of field conservation at the interface!

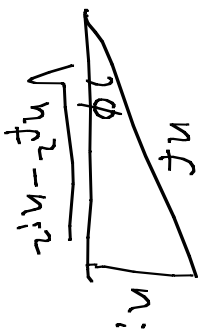
IR application: fiber optics



top surface: $n_f \sin \theta_i^c = n_1 \sin \frac{\pi}{2} \rightarrow \theta_i^c > \theta_i^c = \sin^{-1} \frac{n_1}{n_f}$
 (sides of fiber)

$$\sin \theta_c = \cos \theta_i^c$$

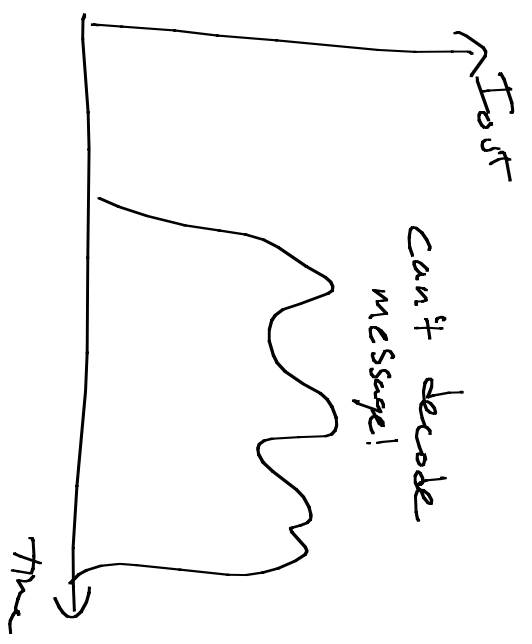
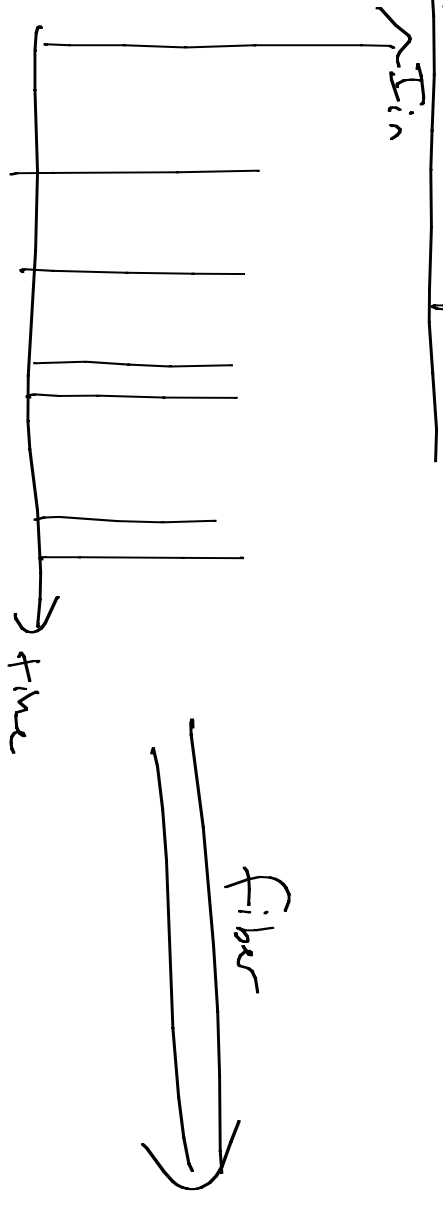
Input interface: $n_1 \sin \theta_i^c = n_f \sin \theta_i^c = n_f \cos \theta_i^c = n_f \cos(\sin^{-1} \frac{n_1}{n_f})$



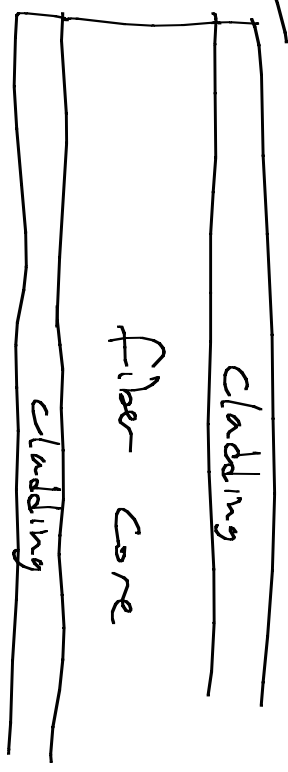
$$n_1 \sin \theta_i^c = n_f \frac{\sqrt{n_f^2 - n_1^2}}{n_f}$$

$$\theta_i^c < \theta_i^c = \sin^{-1} \frac{\sqrt{n_f^2 - n_1^2}}{n_1} = \sin^{-1} \sqrt{\left(\frac{n_f}{n_1}\right)^2 - 1}$$

Intermodal dispersion

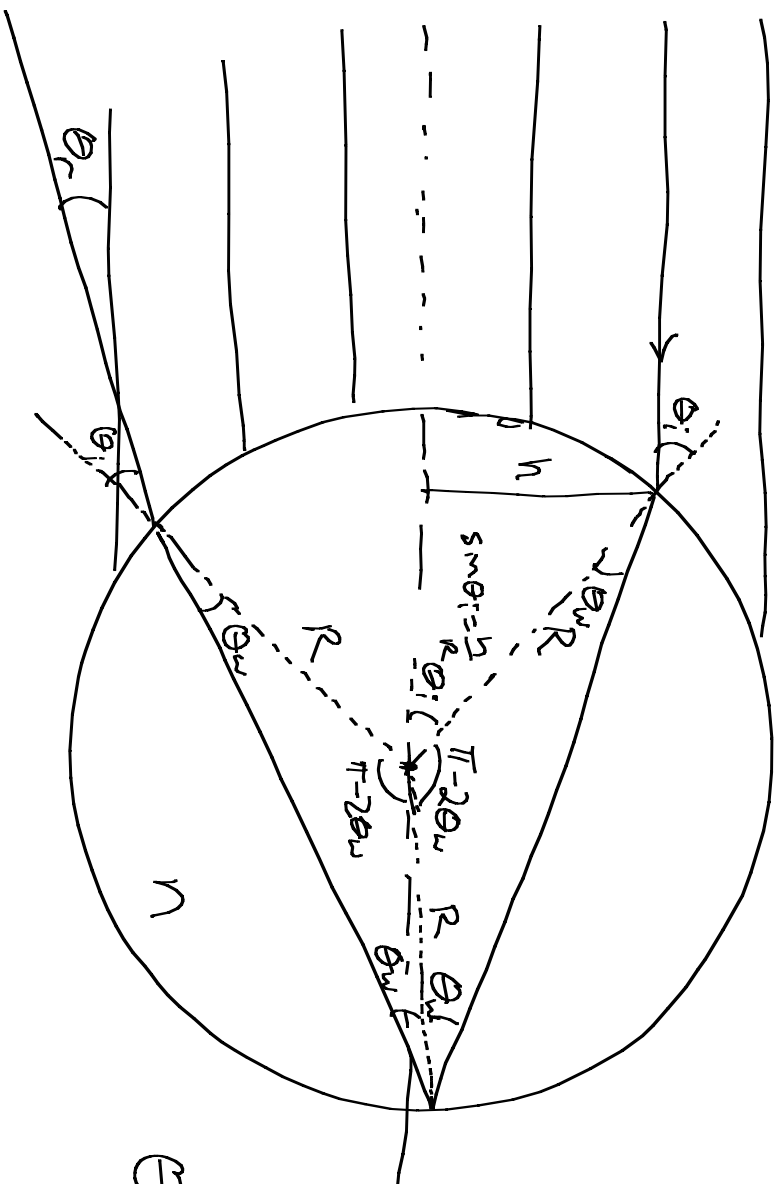


Solution:



$n_{cladding} < n_{core}$
 Reduces θ_i^c and eliminates
 "intermodal dispersion"

Refraction and Reflection in a sphere



$$\sin \theta_i = n \sin \theta_r$$

$$\theta_r = \sin^{-1} \frac{\sin \theta_i}{n}$$

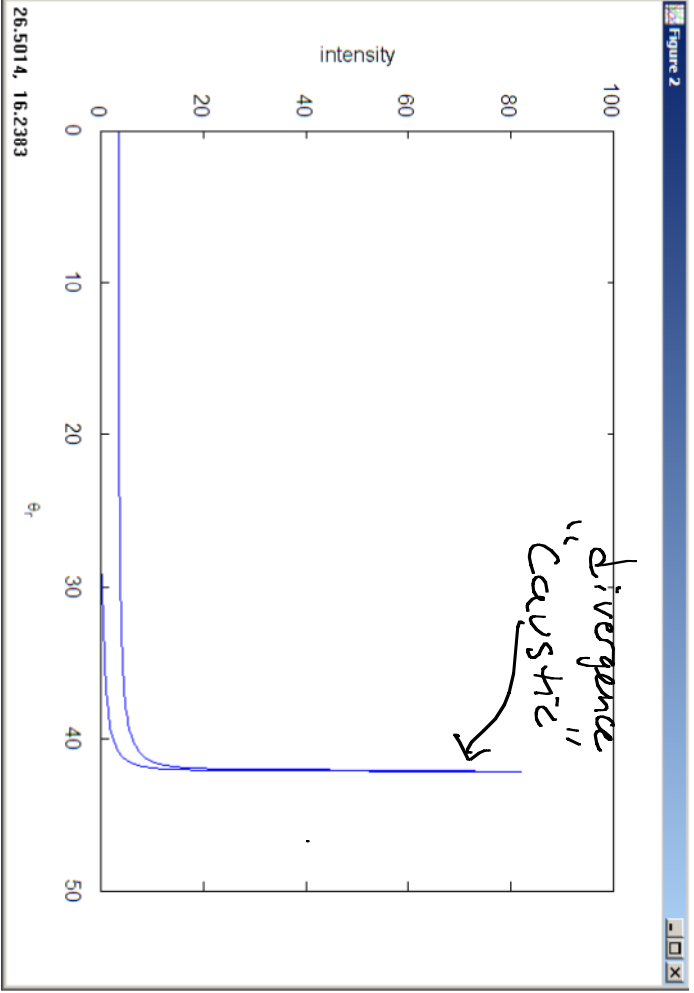
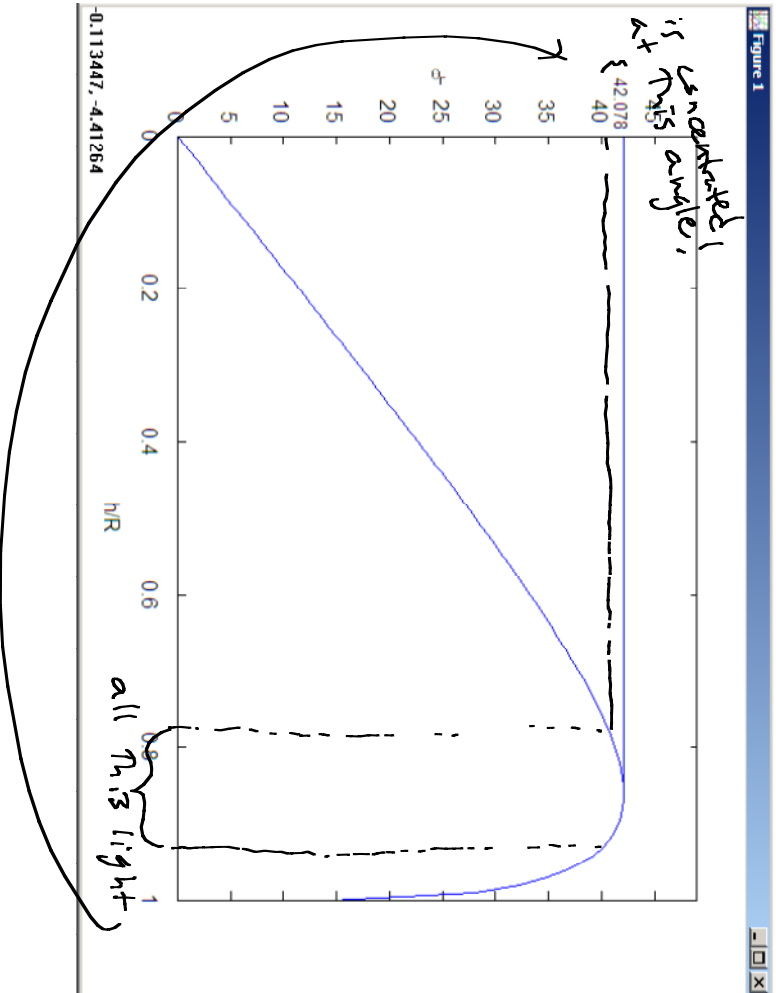
$$\theta_{\text{tot}} = 2(\pi - 2\theta_r) + 2\theta_i$$

$$\theta_r = 2\pi - \theta_{\text{tot}} = 4\theta_r - 2\theta_i$$

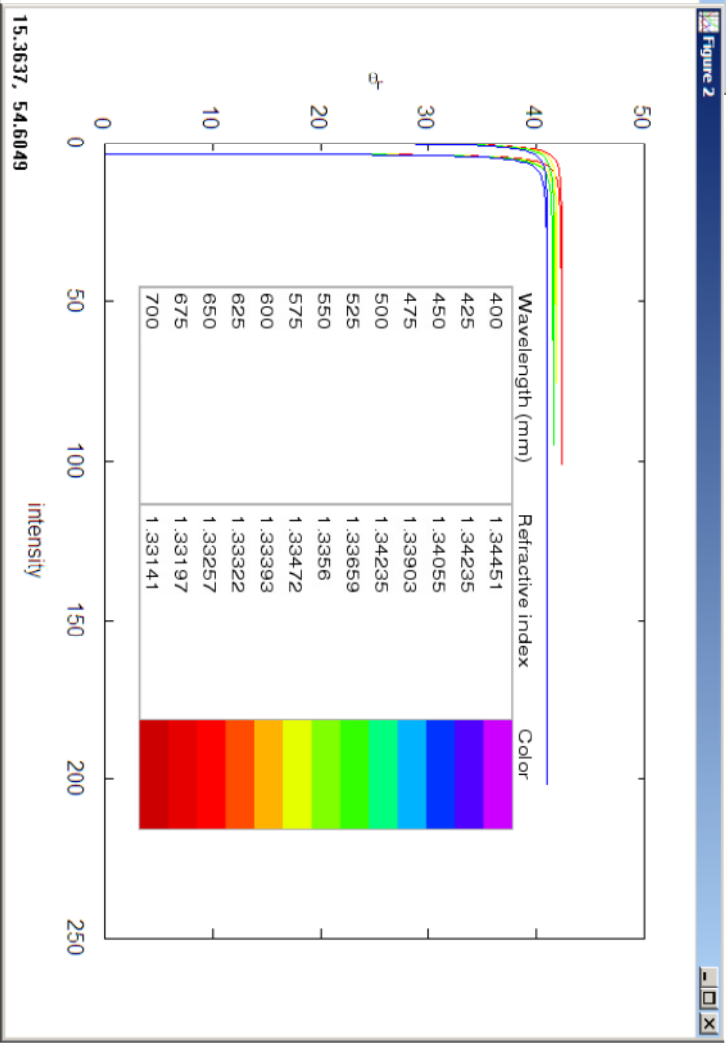
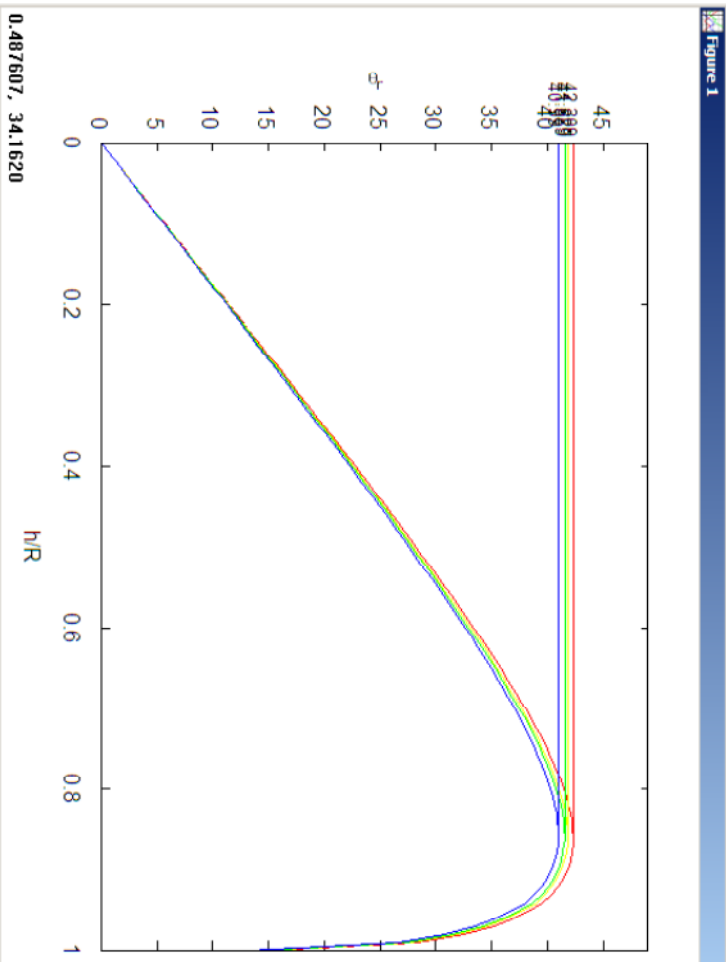
$$= 4 \sin^{-1} \left(\frac{\sin \theta_i}{n} \right) - 2\theta_i$$

$$\theta_i = \sin^{-1} \frac{h}{R}$$

Causatics



Rainbows



← Second rainbow
 from 2 internal
 reflections
 → colors reversed!
 ← primary rainbow